## **Design of experiments for smoke depollution of diesel engine outputs**

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### **ENBIS-EMSE 2009 Conference1st July 2009**





## Talk Overview

- **1. deNOx model: study case**
	- **1.NOx trap: the way it works**
	- **2.NOx trap: the mathematical formulation**
	- **3.NOx trap: experimental and simulated results**
- **2. Kriging with non linear trend (KNL)**
	- **1.Presentation**
	- **2.Kriging predictor**
	- **3. Application on deNOx model and results**
- **3. Conditioning by derivatives: improvement for KNL?**
	- **1.Presentation**
	- **2.Test model: presentation**
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	- **4.First results on deNOx model**

### **Conclusions**





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## **1. NOx trap: the way it works**

## Smoke post-treatment at the diesel engine output: NO<sub>x</sub> trap



engine output





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## **1. NOx trap: the way it works**

Smoke post-treatment at the diesel engine output: NOx trap





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### Reduce pollutants emissions at the diesel engine output



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### **1. NOx trap: the way it works**

**The NOx trap operates in two phases** 

- 1. NOx capture phase until saturation of active sites
- 2. NOx release phase after reducing the oxydated species





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#### **Simplification of the problem**

- • Complex system: to reduce the complexity of the problem, at first, onlycapture phase is considered
- During this phase, the kinetic model have four dominant reactions: •oxydation of CO, HC, NO et  $\mathsf{H}_2$







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#### **Kinetic model**



 $\Rightarrow$  I wo kinetic parameters for each reaction



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### **2. NOx trap: the mathematical formulation**

**Mathematical model** 

The mathematical model of the NOx trap has the form,

$$
Y = f(x, \beta)
$$

where $\boldsymbol{f}$  results from a differential equation system (ODE)





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### **2. NOx trap: the mathematical formulation**

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### **System inputs, denoted by** *x*

On the experimental system, inputs are selected and controlled by the experimenter:

• Mass composition of five species present in the exhaust gas<br> $c_1, c_2, c_3, c_4, c_5$ <br>• Mass flow of gas entering in the NOx trap  $\Omega$ 

*<sup>c</sup>1 , c2 , c3 , c4 , c<sup>5</sup>*

- Mass flow of gas entering in the NOx trap,  $Q$
- $\bullet$  Entering gas temperature  $\Longrightarrow$  increase linearly with the time

$$
x = (c_1, c_2, c_3, c_4, c_5, Q, T)^t
$$





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**System outputs, denoted by** *Y*

Mass composition of the three pollutants:

*yHC , yNOx , yCO*

## **3. NOx trap: experimental and simulated results**



#### **Inadequacy of the computer model**

Kinetic parameter estimation from <sup>a</sup> learning set of 20 experiments

Important differences between computer model and experiments



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#### **2.Kriging with non linear trend (KNL)**

- **1.Presentation**
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## **1. Presentation**

### **Why kriging?**

- 1. To resolve the inadequacy of the mathematical model
- 2. To determine the new experimental points, through variance prediction









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**Kriging with non linear trend**

Differences between computer model and experiments <sup>=</sup> Gaussian process

 $y(x)=f(x,\beta) + z_{\sigma^2,\theta}(x)$ 

where  $z_{\sigma^2\!,\theta}(x)$  is a Gaussian process such as  $\,E(z(x)){=}0$  et  $cov(z(x),z(x{+}h)){=}\sigma^2\!R_\theta(h)$ 





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**Estimation of** β*,* σ*²,* θ

- Estimation by maximum likelihood
	- The analytical formula for  $\beta$  is replaced by a minimization procedure







## **2. Kriging predictor**

**Kriging predictor**

$$
\hat{y}(x_0) = rR^{-1}Y - (F^T R^{-1}r - f)^T (F^T R^{-1}F)^{-1} F^T R^{-1}Y
$$

#### **Notation**

- Let  $m$  be the number of design points
- $Y=(\boldsymbol{Y}_{I},...,\boldsymbol{Y}_{m})^{T}$  output observed at location  $S\text{=}(S_{I},...,S_{m})^{T}$
- $\bullet$   $x_{\textit{0}}^{}$  : point to be predicted
- •*R* : correlation matrix between observations
- •*r* : correlation vector between observations and the point to be predicted
- *F=f(S,* β*)* : value of computer model at design points
- *f=f(x0,*β*)* : value of computer model at the prediction point







## **2. Kriging predictor**

**Kriging predictor**

$$
\hat{y}(x_0) = rR^{-1}Y - (F^T R^{-1}r - f)^T (F^T R^{-1}F)^{-1} F^T R^{-1}Y
$$

**Prediction variance**

$$
\varphi(x_0) = \sigma^2 \left( 1 + \left\| F^T R^{-1} r - f \right\|_{(F^T R^{-1} F)} + \left\| r \right\|_{R} \right)
$$

where  $\|u\|_{-} = u^T A^{-1}$ *A* $u\|_{A} = u^T A^{-1} u$  $=$   $\mu$   $\mu$ 





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where 
$$
||u||_A = u^T A^{-1} u
$$

#### **Parameters estimation**

Parameters are obtained by solving recursively the simultaneous equations:

$$
\hat{\beta} = \min_{\beta} (Y - F)^T R^{-1} (Y - F)
$$

$$
\hat{\sigma}^2 = (Y - F)^T R^{-1} (Y - F) / m
$$

$$
\hat{\theta} = \arg \min [\hat{\sigma}^2 | R^{-1}|^{1/m}]
$$



 $\mathbb{E}$ 

## **3. Application on deNOx model and results**

- **Application**
- •12 experimental points are taken uniformly along the temperature for each of the 19 first experiments

•CO and HC prediction for the 20th experiment, outputs are treated independently





## **3. Application on the deNOx model and results**

**Influence of the number of design point**

 $\bullet$  HC concentration evolution prediction of the 20<sup>th</sup> experiment

• The approach is the same but 15 points are taken uniformly along the temperature instead of 12



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## **1. Presentation**

#### **Notation**

- $\bullet$  Let ( $s_{1},...,s_{m_{I}}$ ) the design points where function value is known
- Let  $(v_1, ..., v_{m_2})$  the design points where partial derivative according to the first direction is known
- Exponent (1) denotes the output derivative along the first direction
- Let,







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- Let  $(v_1, ..., v_{m_2})$  the design points where partial derivative according to the first direction is known
- Exponent (1) denotes the output derivative along the first direction
- Let,

 $Y = (Y_1, ..., Y_{m_1}, Y_1^{(1)}, ..., Y_{m_2}^{(1)})^T$  and  $F = (f(s_1, \beta), ..., f(s_{m_1}, \beta), f^{(1)}(v_1, \beta), ..., f^{(1)}(v_{m_2}, \beta))^T$ 

#### **Covariance structure**

Gaussian spatial correlation is used, defined by,

$$
R(h) = \exp\left\{-\sum_{l=1}^{k} \theta_l h_l^2\right\}
$$

The pairwise joint covariance of  $\pmb{Y}(\pmb{\ldots})$  and  $\pmb{Y}^{(1)}(\pmb{\ldots})$ , is given by,  $_{}$  (Santner, Williams and Notz, 2003)

$$
Cov(Y(s_i), Y^{(1)}(v_j)) = \sigma^2 2\theta_1 (s_i^1 - v_j^1) R(s_i - v_j)
$$
  
\n
$$
Cov(Y^{(1)}(v_i), Y^{(1)}(v_j)) = \sigma^2 (2\theta_1 - 4\theta_1^2 (v_i^1 - v_j^1)^2) R(v_i - v_j)
$$

## **1. Presentation**

**Covariance matrix** *C*

Covariance matrix is defined by,

$$
C = \begin{pmatrix} C_{00} & C_{01} \\ C_{01}^T & C_{11} \end{pmatrix}
$$

where:

•  $C_{00}$  is the  $m_1$ x $m_1$  matrix of correlations between the elements of  $Y_i,$   $\! \leq$   $\! i$   $\!\leq$   $\! m_1$ 

- $C_{0I}$  is the  $m_I$ x $m_2$  matrix of correlations between  $Y_i$  and  $Y_j^{(1)},\ I{\leq}j{\leq}m_2$
- $\bullet$   $\boldsymbol{C}_{11}$  is the  $\boldsymbol{m}_2$ x $\boldsymbol{m}_2$  matrix of correlations between the elements of  $Y_j^{(1)}$





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#### **Kriging equations**

Kriging equations are the same as for kriging with non linear trend





### **2. Test model: presentation**

**Application on two model** 

Kriging with non linear trend conditioning by derivatives (KNLD) is applied on:

- the test model: similar to study case but simpler and totally mastered
- the deNOx model





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**Equations system: represents the experimental system**

Langmuir-Hinshelwood formalization:

$$
\begin{cases}\n\frac{d[A]}{dt} = -\frac{k_0 \exp\{-\frac{E}{RT}\}[A]}{1 + b_0 \exp\{-\frac{\Delta H}{RT}\}[A]}\n\end{cases}
$$
\n
$$
[A]_0 = A_0
$$

Let  $g(x)$  be the model governed by this system





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Let  $g(x)$  be the model governed by this system

#### **Kinetic parameters choice**

• *g(x)* depends on <sup>a</sup> hidden kinetic parameter vector, ξ *={k<sup>o</sup>, E, bo,* ∆*H}*,

• ξ has been chosen to conduct to very different concentration evolutions of A depending on the temperatureEnvironner

## **2. Test model: presentation**

**Second system: represents the mathematical model**

Consider the following simple kinetic system:

$$
\begin{cases}\n\frac{d[A]}{dt} = -k'_0 \exp\{-\frac{E'}{RT}\}[A] \\
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Let *f(x,*β*)* be the model governed by this system, where β*={ko',E'}*





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**Second system: represents the mathematical model**

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Let *f(x,*β*)* be the model governed by this system, where β*={ko',E'}*

### **Objective**

Determine parametersβ*,* <sup>σ</sup>*²,* θ such as:

 $g(x)=f(x, \beta)+z_{\sigma^2,\theta}$ 





## **2. Test model: presentation**

**Simulations**

Simulations for three different  $\mathsf{A}_{0}$  at a fixed time (80 seconds)

Solid line: 'experimental results' (function g), Dotted line: 'estimated model' (f)







### **3. Application on test model and results**

### **Application**

Test model prediction by KNL (red dotted line) and kriging with non linear trend conditioning by derivatives (red solid line) compared to experimental results (blue line)

3 initial concentration, 8 fixed time and 10 temperatures on each simulation









## **4. First results on deNOx model**

### **Application**

- **HC concentration evolution prediction of the 20th experiment by KNL and kriging with non linear trend conditioning by derivatives (KNLD)**
- **15 experimental points taken uniformly along the temperature on the 19 first experiments**
- **On each experimental point function and derivative values are supposed to be known**



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### **Points presented**

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- 2. Kriging with non linear trend conditioning by derivatives (KNLD)







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- Numerical problems when number of design sites increases
	- Oscillations problems where response is less variable







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	- Prediction is better, i.e. oscillations are less strong
	- •Model is too constrained





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### **1. KNL: problems**

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#### **2. KNLD: improvement for KNL**

- Prediction is better, i.e. oscillations are less strong
- •Model is too constrained

### **Perspectives**

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1. Take into account derivative information only on both, initial and final stages for KNLD

Environne

- 2. Determine an experimental design through variance prediction
- 3. Compare this experimental design to classical ones

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## Post-traitement des fumées en sortie des moteurs Diesel : Thank you for your attention!





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